

# 3F1 Signals and Systems: Handout 4

## System transfer function & stability

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Michaelmas Term 2025

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### z-transfer function of an LTIS

A Linear Time-Invariant System (LTIS) described by linear difference equations in canonical form

$$y_k + a_1 y_{k-1} + \dots + a_n y_{k-n} = b_0 x_k + \dots + b_m x_{k-m}$$

and subject to zero initial conditions

$$y_k = x_k = 0 \text{ for } k < 0$$

gives in the z domain

$$Y(z) + a_1 z^{-1} Y(z) + \dots + a_n z^{-n} Y(z) = b_0 X(z) + \dots + b_m z^{-m} X(z)$$

and is hence described by a **transfer function**:

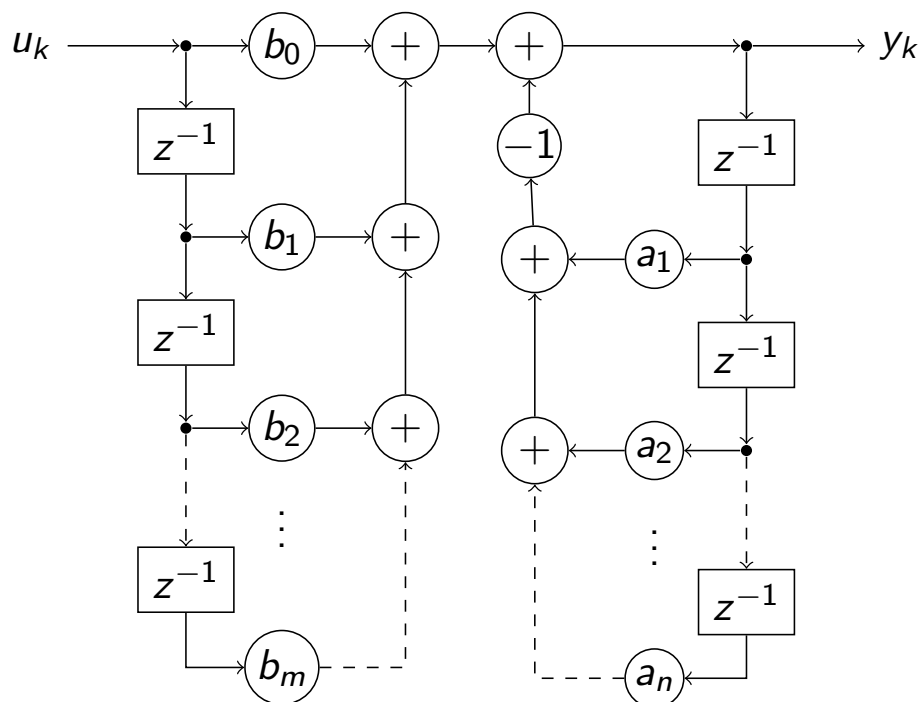
$$G(z) = \frac{Y(z)}{X(z)} = \frac{b_0 + b_1 z^{-1} + \dots + b_m z^{-m}}{1 + a_1 z^{-1} + \dots + a_n z^{-n}}$$

Note: ratio is independent of  $X(z)$ .

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## Direct Form I implementation of an LTIS

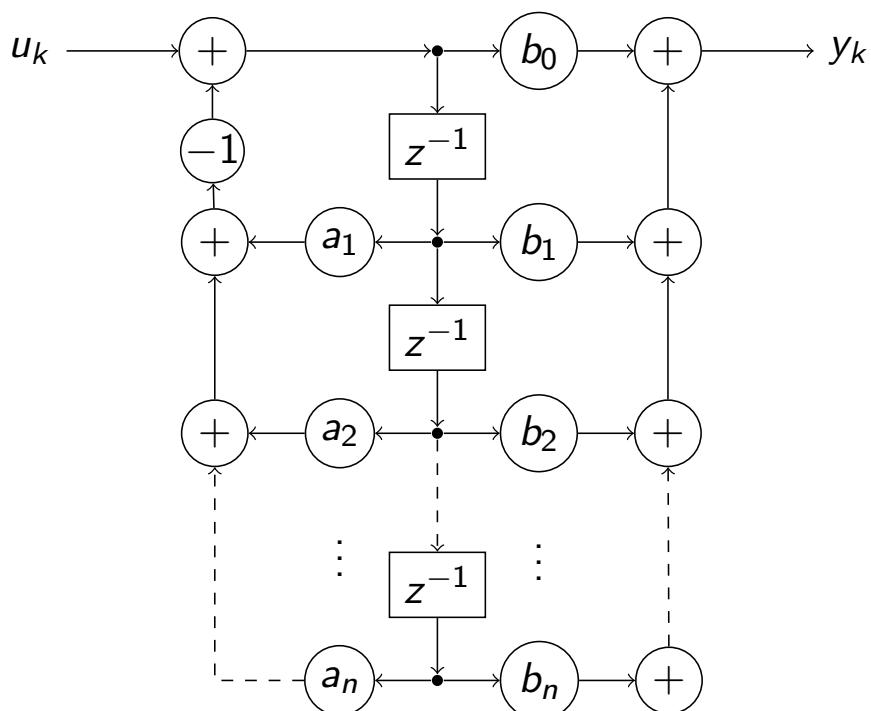
$$G(z) = \frac{b_0 + b_1z^{-1} + \dots + b_mz^{-m}}{1 + a_1z^{-1} + \dots + a_nz^{-n}}$$



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## Direct Form II implementation of an LTIS

$$G(z) = \frac{b_0 + b_1z^{-1} + \dots + b_nz^{-n}}{1 + a_1z^{-1} + \dots + a_nz^{-n}} \text{ where } b_k = 0 \text{ for } k = m+1, \dots, n.$$



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## FIR/IIR in the $z$ domain

- ▶ Direct form II is preferable. The two forms are equivalent because Direct Form I is a cascade of linear systems and you can invert the order of the two systems to obtain Direct Form II (multiplication is commutative)
- ▶ the  $a$  coefficients (denominator of  $G(z)$ ) point in opposite direction from input to output: **feedback**
- ▶ the  $b$  coefficients (numerator of  $G(z)$ ) point in the direction from input to output: **feed-forward**
- ▶ an **FIR** (finite impulse response) satisfies  $a_n = 0$  for all  $n$ , i.e.,  $G(z)$  has only a numerator and a denominator of 1: it's a **feed-forward only system**. The output  $y_k$  only depends on current and past values of the input  $x_k, x_{k-1}, \dots$  but *not* on past values of the output  $y_{k-1}, y_{k-2}, \dots$
- ▶ an **IIR** (infinite impulse response) has an infinite length delta response as a result of **feedback**

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## Poles and Zeros

Switching from negative to positive powers of  $z$ , assuming  $m < n$ ,

$$G(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_m z^{-m}}{1 + a_1 z^{-1} + \dots + a_n z^{-n}} = \frac{b_0 z^n + b_1 z^{n-1} + \dots + b_m z^{n-m}}{z^n + a_1 z^{n-1} + \dots + a_{n-1} z + a_n}$$

or if  $n < m$ ,

$$G(z) = \frac{b_0 z^m + b_1 z^{m-1} + \dots + b_1 z + b_m}{z^n + a_1 z^{n-1} + \dots + a_n z^{m-n}}$$

- ▶ An LTIS in canonical form corresponds to a rational function with equal degrees  $\max\{m, n\}$  in numerator and denominator
- ▶ fundamental theorem of algebra  $\longrightarrow$  every polynomial of degree  $n$  has  $n$  complex roots (counted with multiplicity, i.e., some of them could be co-located)
- ▶ a discrete LTIS has  $\max\{m, n\}$  poles and  $\max\{m, n\}$  zeros
- ▶ for an FIR, all the  $m$  poles are at  $z = 0$

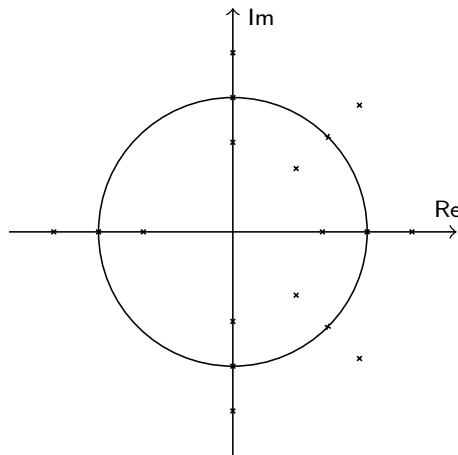
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## Delta response and poles

Consider a (LTI) system  $G(z)$  subjected to a delta input:  
 $\delta_k = (1, 0, 0, \dots) \rightarrow \Delta(z) = 1$ . What is the output?

$$y = \mathcal{Z}^{-1}[Y(z)] = \mathcal{Z}^{-1}[G(z)\Delta(z)] = \mathcal{Z}^{-1}[G(z)]$$

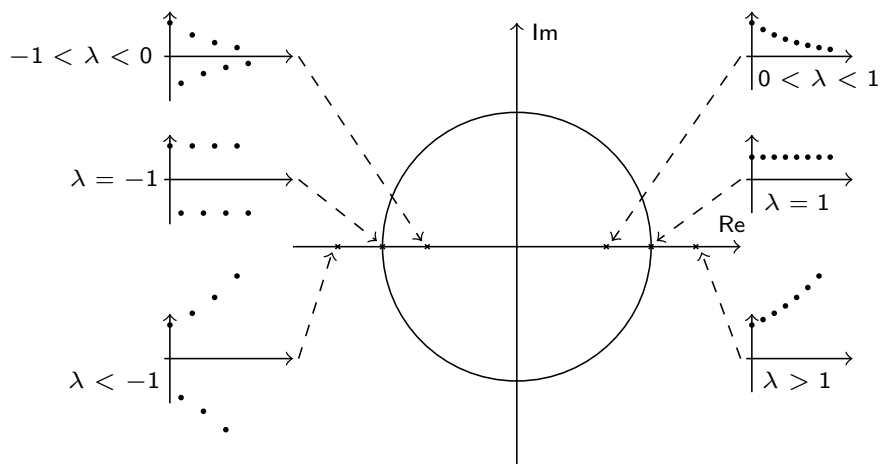
$\Rightarrow$  poles of  $G(z)$  define the response to a pulse



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## Real poles

$$G(z) = \frac{1}{1 - \lambda z^{-1}} \xrightarrow{\mathcal{Z}^{-1}} \lambda^k$$



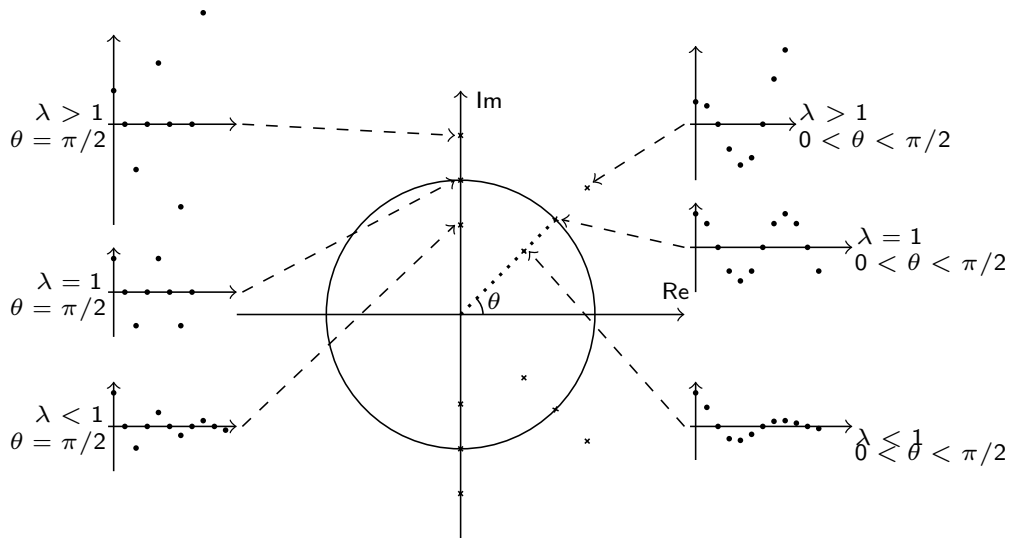
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## Complex conjugate poles

$$G(z) = \frac{1}{1 - (\lambda e^{j\theta})z^{-1}} + \frac{1}{1 - (\lambda e^{-j\theta})z^{-1}}$$

$$\xrightarrow{z^{-1}} \lambda^k (e^{j\theta k} + e^{-j\theta k}) = 2\lambda^k \cos(\theta k)$$

(real impulse response  $\rightarrow$  pair of complex conjugate poles)



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## Repeated poles

►  $G(z) = \frac{1}{(1 - pz^{-1})^2}$

rewrite as  $G(z) = \frac{1}{1 - pz^{-1}} + \frac{pz^{-1}}{(1 - pz^{-1})^2}$  then  $\xrightarrow{z^{-1}} p^k + kp^k$

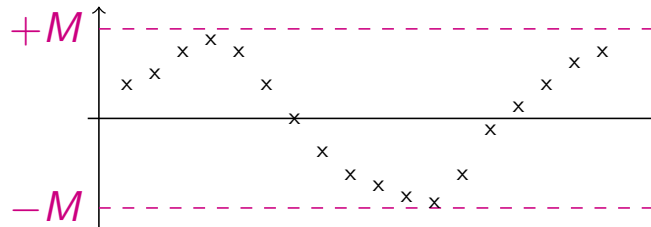
## Damping and Oscillation

- distance of poles from origin is a measure of decay rate
- complex poles just inside unit circle give lightly damped oscillation
- oscillation is possible for real poles on negative real axis

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# Bounded signals

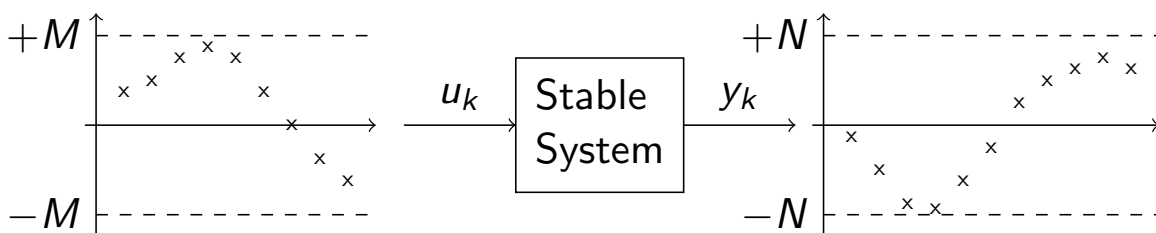
We say that a signal  $\{u_k\}$  is **bounded** if there exists a positive constant  $M$  such that  $|u_k| < M$  for all  $k$ .



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## BIBO Stability

A discrete time system is **stable** if bounded inputs give bounded outputs (“BIBO” stability).



For any constant  $M$ , there exists a constant  $N$  such that, for any input signal bounded by  $M$  the output is bounded by  $N$ .

- ▶ The definition is more subtle than appears:
  - ▶ If a bounded input gives an unbounded output, the system is unstable
  - ▶ However, for some unstable systems there is no unbounded output but a collection of input signals bounded by  $M$  give outputs that cannot be bounded by any single  $N$  (See Examples Paper 1)

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## Theorem (Conditions for stability of a discrete time system)

Let  $G$  be a discrete time system with a rational transfer function,

$$G(z) = \frac{b(z)}{a(z)} = \frac{b_0 + \dots + b_m z^{-m}}{1 + a_1 z^{-1} + \dots + a_n z^{-n}}$$

with no common factors between  $b(z)$  and  $a(z)$ . Let the pulse response of  $G$  be  $\{g_k\}_{k \geq 0}$ . Then the following are equivalent:

1.  $G$  is stable
2. All of the roots  $p_i$  of  $a(z)$  (i.e. poles) satisfy  $|p_i| < 1$
3.  $\sum_{k=0}^{\infty} |g_k|$  is finite

Logical sequence of proof:

$$(1) \xrightarrow{A} (2) \xrightarrow{\text{Ex. paper}} (3) \xrightarrow{B} (1)$$

(Moreover, Example sheet shows  $1 \implies 3$  and re-visits  $1 \implies 2$  with real input signals .)

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## Reminder: logic and mathematical proofs

- ▶  $A \implies B$  means that if  $A$  is true, then  $B$  is true. The reverse doesn't necessarily hold: it is possible for  $B$  to be true but  $A$  to be false. For example
  - ▶  $x = 2 \implies x^2 = 4$
  - ▶ but  $x^2 = 4 \not\implies x = 2$  ( $x$  could be  $-2!$ )
- ▶ Implication is transitive:  $A \implies B \implies C$  implies  $A \implies C$
- ▶ Equivalence:  $A \iff B$  means  $A \implies B$  and  $B \implies A$ , also known as "if and only if":  $A$  is true if and only if  $B$  is true.
- ▶ To prove equivalence, you need to prove the two implications, i.e.,  $A \implies B$  and  $B \implies A$
- ▶  $A \implies B$  is equivalent to  $\neg B \implies \neg A$ , where  $\neg$  is the negation operator ("not  $B$  implies not  $A$ "). Often it is easier to prove  $\neg B \implies \neg A$  than  $A \implies B$ , but since these statements are equivalent, the proof is equally valid.

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## Proof, part A

A:  $G$  stable  $\implies$  all of the roots of  $a(z)$  satisfy  $|p_i| < 1$ .

We will prove  $\neg(|p_i| < 1 \text{ for all } i) \implies G$  not stable, i.e., **if there is at least one root for which  $|p_i| \geq 1$ , then  $G$  is not stable.**

Suppose  $p_1, p_2, p_3, \dots$  are distinct. Then we can decompose  $G$  using partial fractions:

$$G(z) = \frac{\alpha_1}{1 - p_1 z^{-1}} + \dots + \frac{\alpha_n}{1 - p_n z^{-1}}$$

Then

$$g_k = \alpha_1 p_1^k + \alpha_2 p_2^k + \dots + \alpha_n p_n^k$$

Suppose  $|p_i| > 1$  for some  $i$ . Then  $g_k$  is unbounded.

Therefore **a delta input (bounded) gives an unbounded output and hence  $G$  is not stable.**

The proof with repeated poles is more involved but follows similar lines.

What about if there is no pole such that  $|p_i| > 1$  but **a pole with  $|p_i| = 1$ ?**

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## Pole on the unit circle

$$G(z) = \frac{\alpha_i}{1 - e^{j\theta} z^{-1}} + \tilde{G}(z)$$

where  $\tilde{G}(z)$  contains the remaining terms in the partial fraction expansion of  $G(z)$ . Recall that  $g_k = \alpha_1 p_1^k + \dots + \alpha_n p_n^k$  and hence the  $i$ -th term in the sum corresponding to this pole is

$$g'_k = \alpha_i e^{j\theta k}$$

whose magnitude  $|g'_k| = \alpha_i$  is constant for all times and hence bounded.

Now consider the input

$$U(z) = \frac{\alpha_i z^{-1}}{1 - e^{j\theta} z^{-1}}.$$

It corresponds to the sequence  $g'_{k-1}$  as it is simply the time-shift operator  $z^{-1}$  applied to the  $z$  transform of  $g'_k$ , and hence it is bounded.

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## Pole on the unit circle (continued)

The corresponding output is

$$\begin{aligned} Y(z) &= U(z)G(z) = U(z) \left( \frac{\alpha_i}{1 - e^{j\theta}z^{-1}} + \tilde{G}(z) \right) \\ &= \frac{\alpha_i^2 z^{-1}}{(1 - e^{j\theta}z^{-1})^2} + U(z)\tilde{G}(z) \end{aligned}$$

The first term in this sum corresponds to the time sequence

$$y'_k = k\alpha_i^2 e^{j\theta(k-1)}$$

whose magnitude grows with  $k$  and is therefore unbounded! Hence we have found a bounded input  $g'_{k-1}$  that gives an output  $y_k$  with an unbounded component  $y'_k$ .

We have completed the proof that

$$G(z) = \frac{b(z)}{a(z)} \text{ is stable} \implies \text{the roots of } a(z) \text{ satisfy } |p_i| < 1$$

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## Proof, part B

B:  $\sum_{k=0}^{\infty} |g_k| < \infty \implies G \text{ stable (b. input} \implies \text{b. output)}$

Suppose that  $\sum_{k=0}^{\infty} |g_k| < \infty$ , i.e., the sum is finite. Let  $\{u_k\}$  be an arbitrary **bounded** input, i.e.  $|u_k| < M$  for  $k \geq 0$ . Then the output,  $\{y_k\}$  is given by the convolution

$$y_k = \sum_{i=0}^k g_i u_{k-i}$$

Thus,

$$\begin{aligned} |y_k| &= \left| \sum_{i=0}^k g_i u_{k-i} \right| \\ &\leq \sum_{i=0}^k |g_i| |u_{k-i}| \\ &< \sum_{i=0}^k |g_i| M = M \sum_{i=0}^k |g_i| < \infty \end{aligned}$$

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